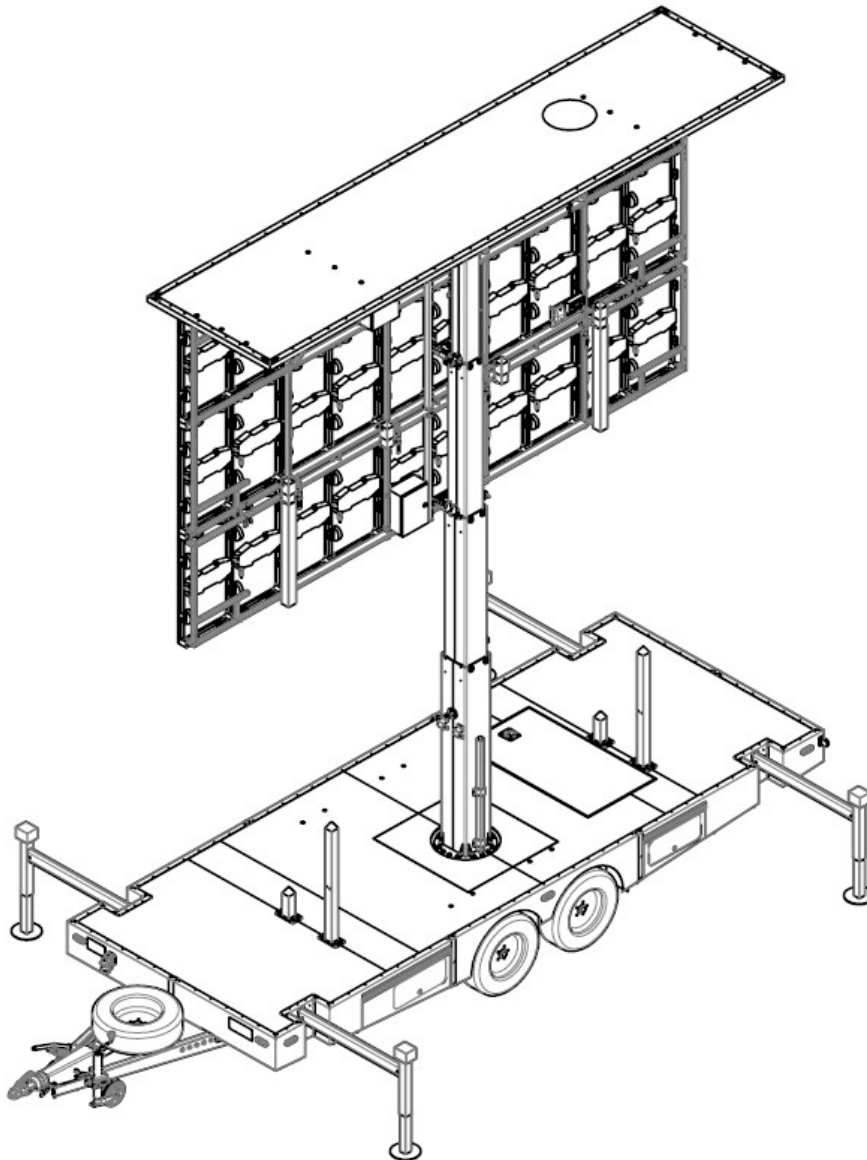


Calculation of static

Trailer PlatformLED 15m²



Inowrocław, P15AUD-2

12.06.2024

1. Introduction

There is a description in this document of analysis performed to check operating limitations during use of this machine:

- Determination of critical and safe (stable) wind speed and reactions in supports.
- Determination of wind speed limits as a result of stress in construction

Calculations were performed based on the analytical method and FEM (Finite-element method) method.

2. Calculations

Two cases of load were considered due to screen setting, and wind direction (Fig. 2.1).

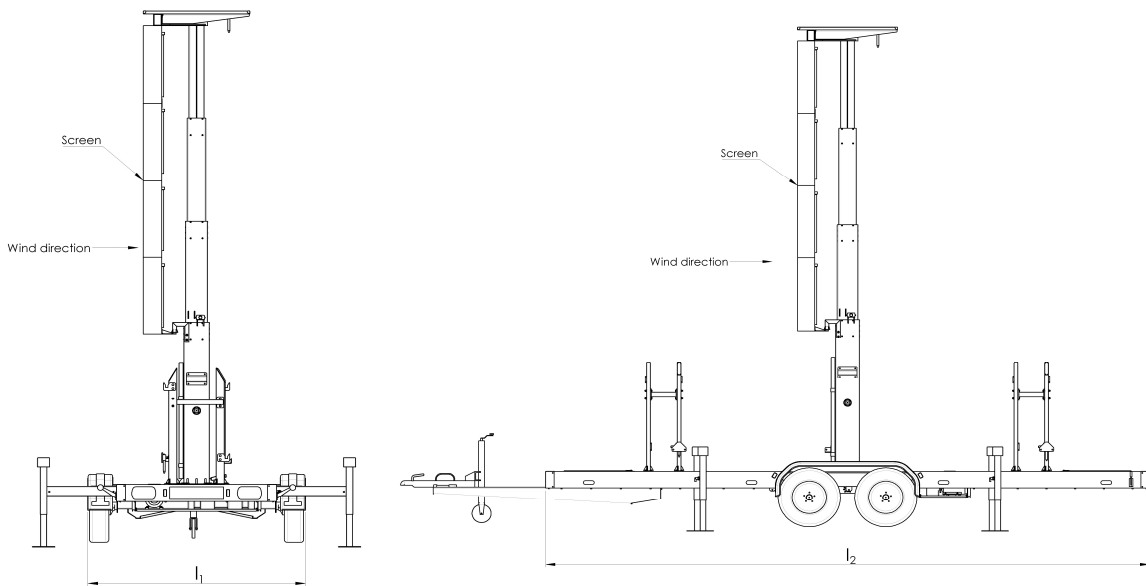


Fig. 2.1. Cases of loads due to wind direction and screen setting.

2.1 The first load case - wind blowing from the side

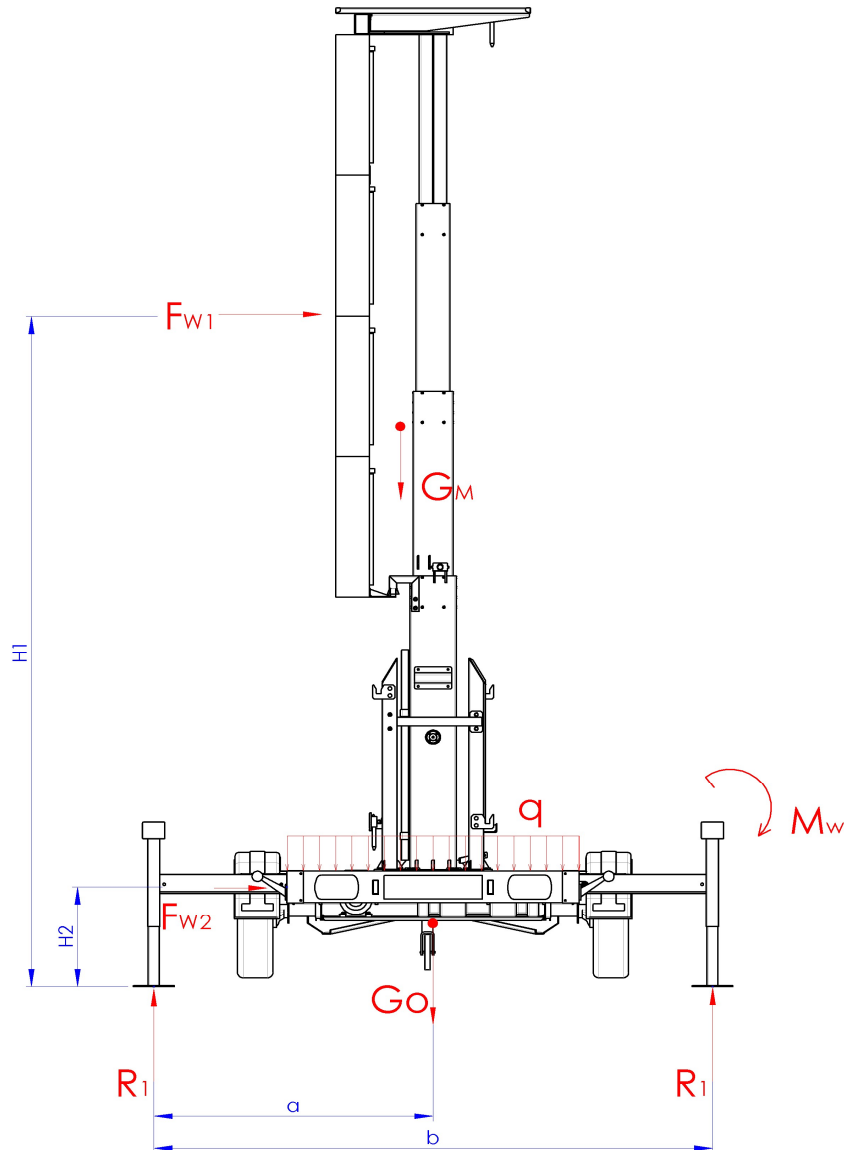


Fig. 2.2. The first load case-distribution of forces and torques.

Drawing reference:

- R_1 - reaction in the first support(windward)
- R_2 - reaction in the second support(leeward)
- G_0 - axle weight
- q - construction weight (frame, container, instrumentation)
- G_M - mast weight
- F_{w1} - wind force on the screen
- F_{w2} - wind force on the side surface of the container
- M_w - resultant torque of wind

Calculation constants	
Acceleration due to gravity [m/s ²]	9,81
Partial safety factor	1,35
Wind safety factor	1,2
Aerodynamic coefficient	1,8
Friction μ (sand,gravel-wood)	0,65
Friction μ (wood-concrete)	0,6
Field point for steel 355 fy [MPa]	355
Safety factor (yield) γ	1,1

Weight of components and generated loads			
	Weight [kg]	Load [N]	Shown in Fig. 2.2.
Mast+screen	1200	11772	G_M
Frame+container+instrumentation	1600	15696	p
Axle	230	2256,3	$2G_O$
Catch	80	784,8	G_c
The total weight of the trailer N_k	3110	30509,1	

Dimensions [mm] (Fig. 2.2)	
a	1819
b	4100
l2	5500
H1	5407
H2	380
H3	1600

Surfaces	
Screen A_{ref1} [m ²]	15
Side surface of the container A_{ref2} [m ²]	2,5
Screen retracted	15

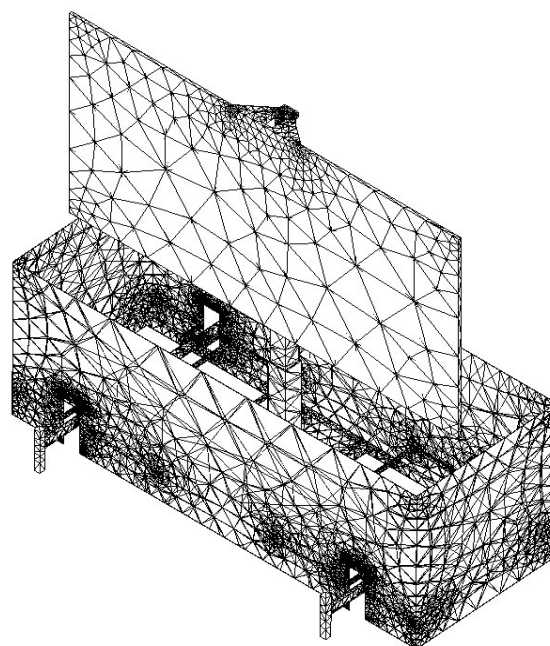


Fig.2.3. Discrete model for FEM calculation

Wind loads according to EN 13814:

$$F_w = q_{eq} \times c_f \times A_{ref}$$

$$v_{ref} = 15 \frac{m}{s} \rightarrow q_{eq} = q_{req} \times c_e(z_e) \times c_d = 0,2 \frac{kN}{m^2}$$

$$v_{ref} = 28 \frac{m}{s} \rightarrow q_{eq} = q_{req} \times c_e(z_e) \times c_d = 0,35 \frac{kN}{m^2}$$

Verification of stability:

The safety against overturning according to EN 13814:

$$\Sigma \gamma M_{St,k} \geq \Sigma \gamma M_{K,k}$$

$$\Sigma \gamma M_{St,k} = a \cdot (G_M + 2G_0 + G_c + q)$$

$$= 1819 \cdot (11772 + 15696 + 2256 + 785) / 1000000$$

$$= \mathbf{55,5 \text{ kNm}}$$

LED screen ON

$$\Sigma \gamma M_{K,k} = \gamma \Sigma F_W \cdot H_i$$

$$= 1,2 \cdot (0,2 \cdot 1,8 \cdot 15 \cdot 5407 / 1000 + 0,2 \cdot 1,8 \cdot 2,5 \cdot 380 / 1000)$$

$$= \mathbf{35,4 \text{ kNm}}$$

LED screen OFF

$$\Sigma \gamma M_{K,k} = \gamma \Sigma F_W \cdot H_i$$

$$= 1,2 \cdot (0,56 \cdot 1,8 \cdot 15 \cdot 1600 / 1000)$$

$$= \mathbf{29,0 \text{ kNm}}$$

LED screen OFF for 15m²

$$= 1,2 \cdot (0,56 \cdot 1,8 \cdot 15 \cdot 1600 / 1000)$$

$$= \mathbf{29,0 \text{ kNm}}$$

Condition of stability			
LED screen ON, Vref=15m/s	55,5	≥	35,4
LED screen OFF, Vref=28m/s	55,5	≥	29,0
LED screen OFF 15m ²	55,5	≥	29,0

The safety against sliding according to EN 13814:

$$\Sigma\gamma\mu N_k \geq \Sigma\gamma H_k$$

$$\mu = 0,65$$

$$\Sigma\gamma\mu N_k = 0,65 \cdot 30509 = \mathbf{19,8 \text{ kN}}$$

$$\mu = 0,6$$

$$\Sigma\gamma\mu N_k = 0,6 \cdot 30509 = \mathbf{18,3 \text{ kN}}$$

LED screen ON

$$\begin{aligned} \Sigma\gamma H_k &= 1,2 \cdot 0,2 \cdot 1,8 \cdot (15 + 2,5) \\ &= \mathbf{7,56 \text{ kN}} \end{aligned}$$

LED screen OFF

$$\begin{aligned} \Sigma\gamma H_k &= 1,2 \cdot 0,35 \cdot 1,8 \cdot 15 \\ &= \mathbf{11,3 \text{ kN}} \end{aligned}$$

Condition safety against sliding			
LED screen ON, Vref=15m/s, $\mu=0,65$	19,8	\geq	7,6
LED screen OFF, Vref=28m/s, $\mu=0,65$	19,8	\geq	11,3
LED screen ON, Vref=15m/s, $\mu=0,6$	18,3	\geq	7,6
LED screen OFF, Vref=28m/s, $\mu=0,6$	18,3	\geq	11,3

The structural strength was calculated against load case from wind vref=15m/s and LED screen ON (like in Fig 2.2) using FEM.

Load combinations and allowable stress was determined according to EN 13814.

2.2 The second load case - wind blowing from the front

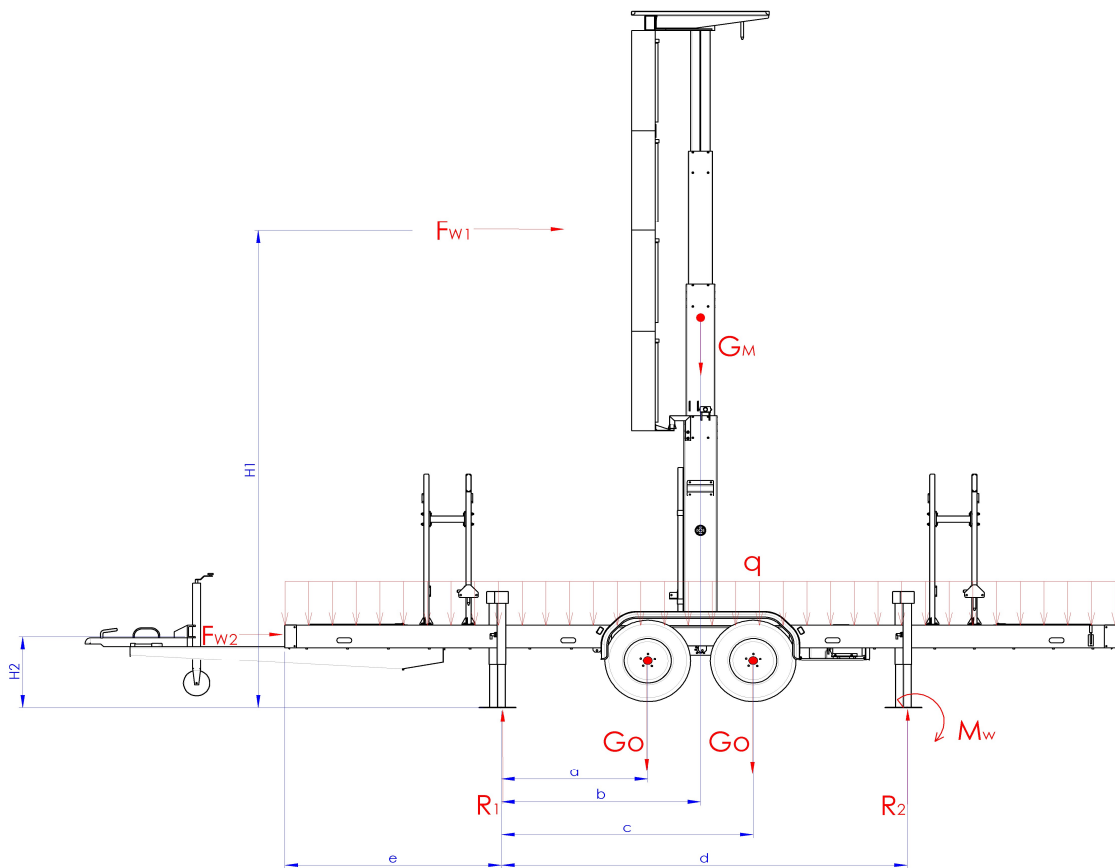


Fig.2.4. Second load case – distribution of forces and torques.

Drawing reference:

- R_1 - reaction in the first support (windward)
- R_2 - reaction in the second support (leeward)
- G_0 - axle weight
- q - construction weight (frame, container, instrumentation)
- G_M - mast weight
- F_{w1} - wind force on the screen
- F_{w2} - wind force on the side surface of the container
- M_w - resultant torque of wind

Calculation constants	
Acceleration due to gravity [m/s ²]	9,81
Partial safety factor	1,35
Wind safety factor	1,2
Aerodynamic coefficient	1,8
Friction μ (sand,gravel-wood)	0,65
Friction μ (wood-concrete)	0,6
Field point for steel 355 fy [MPa]	355
Safety factor (yield) γ	1,1

Weight of components and generated loads			
	Weight [kg]	Load [N]	Shown in Fig. 2.2.
Mast+screen	1200	11772	G_M
Frame+container+instrumentation	1600	15696	p
Axle	230	2256,3	$2G_O$
Catch	80	784,8	G_c
The total weight of the trailer N_k	3110	30509,1	

Dimensions [mm] (Fig. 2.4)	
a	1930
b	2330
c	2730
d	4600
e	424
l_1	2200
H1	5407
H2	380
H3	1600

Surfaces	
Screen A_{ref1} [m ²]	15
Side surface of the container A_{ref2} [m ²]	1
Screen retracted	15

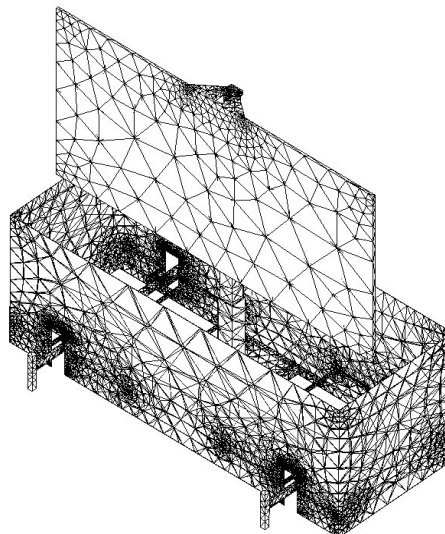


Fig.2.5. Discrete model for FEM calculation

Wind loads according to EN 13814:

$$F_w = q_{eq} \times c_f \times A_{ref}$$

$$v_{ref} = 15 \frac{m}{s} \rightarrow q_{eq} = q_{req} \times c_e(z_e) \times c_d = 0,2 \frac{kN}{m^2}$$

$$v_{ref} = 28 \frac{m}{s} \rightarrow q_{eq} = q_{req} \times c_e(z_e) \times c_d = 0,35 \frac{kN}{m^2}$$

Verification of stability:

The safety against overturning according to EN 13814:

$$\Sigma \gamma M_{St,k} \geq \Sigma \gamma M_{K,k}$$

$$\Sigma \gamma M_{St,k} = (d - b) \cdot (G_M + 2G_0 + q) + (e + d) \cdot G_C$$

$$= 71,4 \text{ kNm}$$

LED screen ON

$$\Sigma \gamma M_{K,k} = \gamma \Sigma F_W \cdot H_i$$

$$= 1,2 \cdot (0,2 \cdot 1,8 \cdot 15 \cdot 5407 / 1000 + 0,2 \cdot 1,8 \cdot 1 \cdot 380 / 1000)$$

$$= 35,2 \text{ kNm}$$

LED screen OFF

$$\Sigma \gamma M_{K,k} = \gamma \Sigma F_W \cdot H_i$$

$$= 1,2 \cdot (0,56 \cdot 1,8 \cdot 15 \cdot 1600 / 1000)$$

$$= 29,0 \text{ kNm}$$

LED screen OFF 14m²

$$= 355 \cdot (0,56 \cdot 1,8 \cdot 15 \cdot 1600 / 1000)$$

$$= 29,0 \text{ kNm}$$

Condition of stability			
LED screen ON, Vref=15m/s	71,4	≥	35,2
LED screen OFF, Vref=28m/s	71,4	≥	29,0
LED screen OFF 14m ²	71,4	≥	29,0

The safety against sliding according to EN 13814:

$$\Sigma\gamma\mu N_k \geq \Sigma\gamma H_k$$

$$\mu = 0,65$$

$$\Sigma\gamma\mu N_k = 0,65 \cdot 30509 = \mathbf{19,8 \text{ kN}}$$

$$\mu = 0,6$$

$$\Sigma\gamma\mu N_k = 0,6 \cdot 30509 = \mathbf{18,3 \text{ kN}}$$

LED screen ON

$$\begin{aligned} \Sigma\gamma H_k &= 1,2 \cdot 0,2 \cdot 1,8 \cdot (15 + 1) \\ &= \mathbf{6,9 \text{ kN}} \end{aligned}$$

LED screen OFF

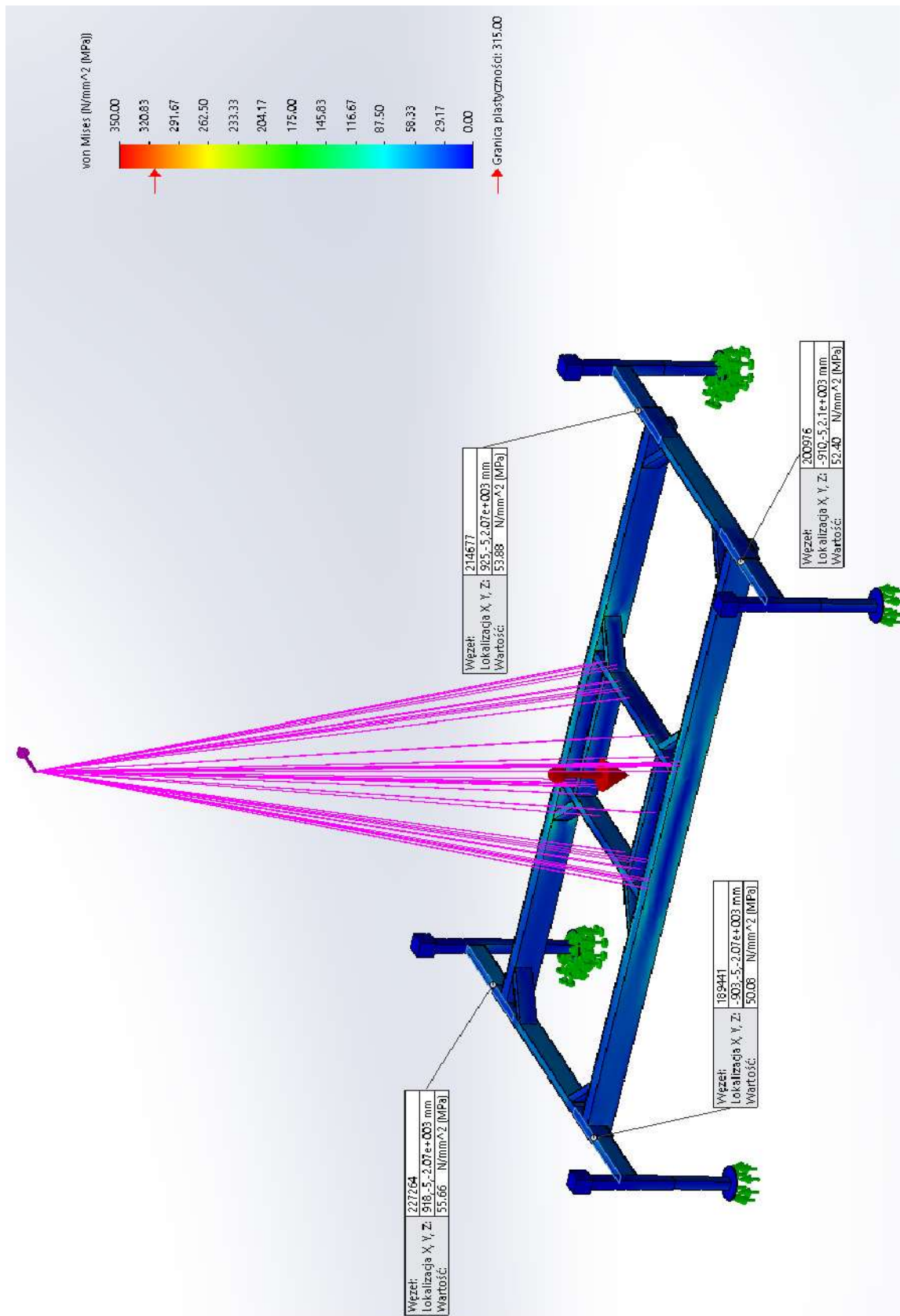
$$\begin{aligned} \Sigma\gamma H_k &= 1,2 \cdot 0,35 \cdot 1,8 \cdot 15 \\ &= \mathbf{11,3 \text{ kN}} \end{aligned}$$

Condition safety against sliding			
LED screen ON, Vref=15m/s, $\mu=0,65$	19,8	\geq	6,9
LED screen OFF, Vref=28m/s, $\mu=0,65$	19,8	\geq	11,3
LED screen ON, Vref=15m/s, $\mu=0,6$	18,3	\geq	6,9
LED screen OFF, Vref=28m/s, $\mu=0,6$	18,3	\geq	11,3

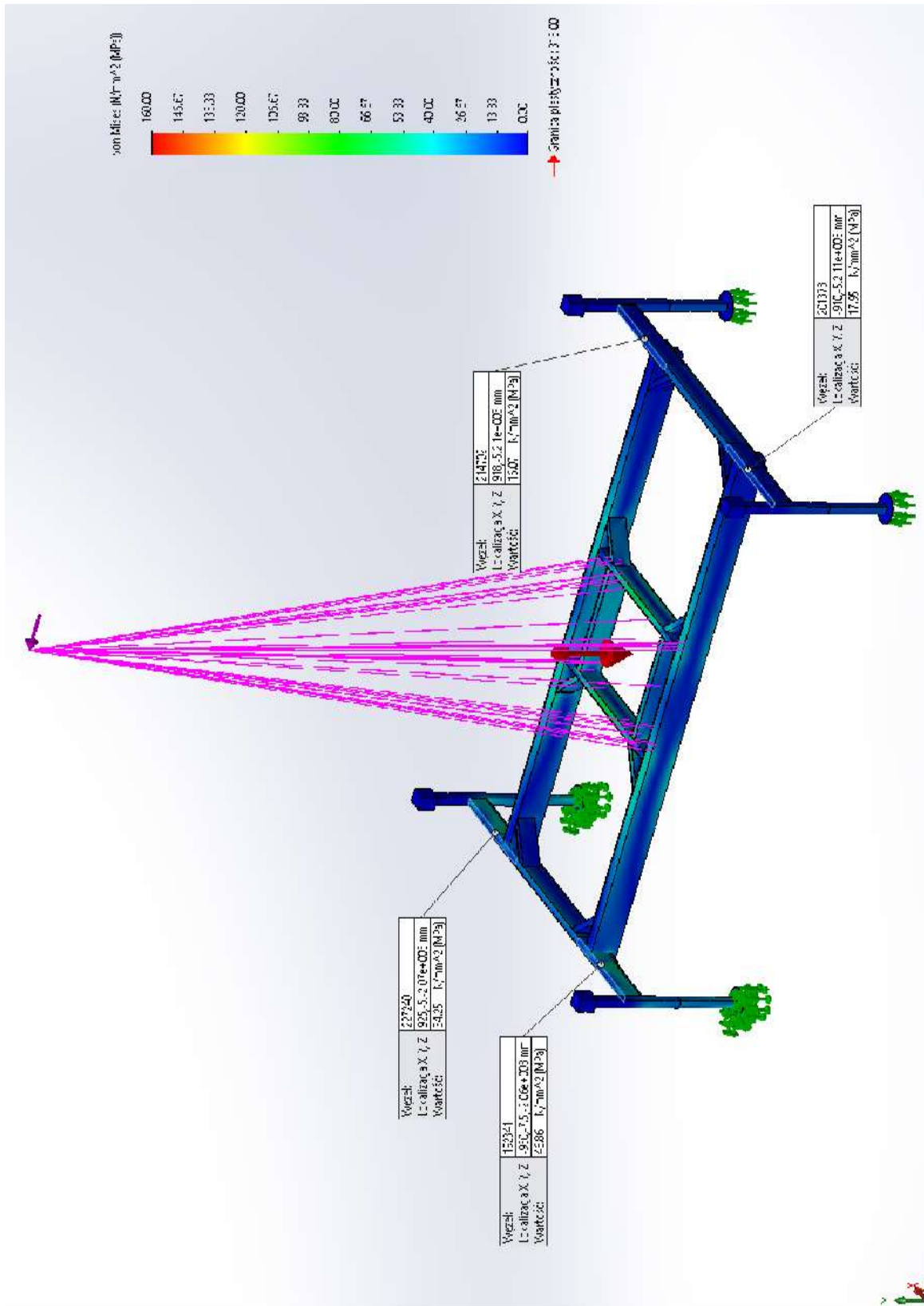
The structural strength was calculated against load case from wind vref=15m/s and LED screen ON (like in Fig 2.2) using FEM.

Load combinations and allowable stress was determined according to EN 13814.

Wind blowing from the site



Wind blowing from the front



3. Conclusion

In this study there has been performed an analysis of the trailer with the screen against various operating conditions in order to validate the stability of the construction. Calculations, both analytical and finite-element method (FEM), have been implemented for that purpose.

- The trailer can be operated safely at the wind speed up to 15m/s;
- The trailer is safe at the wind speed up to 28m/s in LED screen OFF position (screen retracted)